**3GPP TSG RAN WG1 #120bis *R1-250xxxx***

**Wuhan, China, April 7th – 11th, 2025**

|  |
| --- |
| *CR-Form-v12.2* |
| **CHANGE REQUEST** |
|  |
|  | **38.901** | **CR** | **Draft** | **rev** |  | **Current version:** | **18.0.0** |  |
|  |
| *For* [***HE******LP***](http://www.3gpp.org/3G_Specs/CRs.htm#_blank)*on using this form: comprehensive instructions can be found at* [*http://www.3gpp.org/Change-Requests*](http://www.3gpp.org/Change-Requests)*.* |
|  |

|  |  |  |  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- | --- | --- | --- |
| ***Proposed change affects:*** | UICC apps |  | ME | **X** | Radio Access Network | **X** | Core Network |  |

|  |
| --- |
|  |
| ***Title:***  | Draft CR to introduce channel model for ISAC |
|  |  |
| ***Source to WG:*** | Xiaomi, AT&T |
| ***Source to TSG:*** | R1 |
|  |  |
| ***Work item code:*** | FS\_Sensing\_NR |  | ***Date:*** | 2025-4-7 |
|  |  |  |  |  |
| ***Category:*** | B |  | ***Release:*** | Rel-19 |
|  | *Use one of the following categories:****F*** *(correction)****A*** *(mirror corresponding to a change in an earlier release)****B*** *(addition of feature),* ***C*** *(functional modification of feature)****D*** *(editorial modification)*Detailed explanations of the above categories canbe found in 3GPP [TR 21.900](http://www.3gpp.org/ftp/Specs/html-info/21900.htm). | *Use one of the following releases:Rel-8 (Release 8)Rel-9 (Release 9)Rel-10 (Release 10)Rel-11 (Release 11)…Rel-16 (Release 16)Rel-17 (Release 17)Rel-18 (Release 18)Rel-19 (Release 19)* |
|  |  |
| ***Reason for change:*** | In RAN #102, the study item for channel modelling for ISAC was agreed. The output of the study item was agreed to be incorporated into TR 38.901. This CR captures the agreements/conclusions of the study item for channel modelling for ISAC. |
|  |  |
| ***Summary of change:*** | New clauses, i.e., 7.9 and [8.1] are added for the channel model for ISAC. The existing sections 1, 2, 4, […] are also updated to reflect the introduction of channel model for ISAC.  |
|  |  |
| ***Consequences if not approved:*** | The existing channel model for communications in TR 38.901 is not sufficient to address evaluation of sensing techniques for Integrated Sensing and Communications use cases. The existing models in TR38.901 are not designed for sensing, in particular they do not address target modelling and sensing, background environment modelling and differentiation from targets.  |
|  |  |
| ***Clauses affected:*** | Impact to all/most clauses expected |
|  |  |
|  | **Y** | **N** |  |  |
| ***Other specs*** |  | **X** |  Other core specifications  | TS/TR ... CR ...  |
| ***affected:*** |  | **X** |  Test specifications | TS/TR ... CR ...  |
| ***(show related CRs)*** |  | **X** |  O&M Specifications | TS/TR ... CR ...  |
|  |  |
| ***Other comments:*** |  |
|  |  |
| ***This CR's revision history:*** |  |

# 1 Scope

The present document captures the findings of the study item, "Study on channel model for frequency spectrum above 6 GHz" [2] and from further findings of the study item, "Study on New Radio Access Technology [22]", the study item "Study on Channel Modeling for Indoor Industrial Scenarios [23]" and the study item "Study on channel modelling for Integrated Sensing And Communication (ISAC) for NR [24]". The channel models in the present document address the frequency range 0.5-100 GHz. The purpose of this TR is to help TSG RAN WG1 to properly model and evaluate the performance of physical layer techniques using the appropriate channel model(s). Therefore, the TR will be kept up-to-date via CRs in the future.

This document relates to the 3GPP evaluation methodology and covers the modelling of the physical layer of both Mobile Equipment and Access Network of 3GPP systems.

This document is intended to capture the channel model(s) for frequencies from 0.5GHz up to 100GHz.

# 2 References

The following documents contain provisions which, through reference in this text, constitute provisions of the present document.

- References are either specific (identified by date of publication, edition number, version number, etc.) or non‑specific.

- For a specific reference, subsequent revisions do not apply.

- For a non-specific reference, the latest version applies. In the case of a reference to a 3GPP document (including a GSM document), a non-specific reference implicitly refers to the latest version of that document *in the same Release as the present document*.

[1] 3GPP TR 21.905: "Vocabulary for 3GPP Specifications".

[2] 3GPP TD RP-151606: "Study on channel model for frequency spectrum above 6 GHz".

[3] 3GPP TR 36.873 (V12.2.0): "Study on 3D channel model for LTE".

[4] 3GPP RP-151847: "Report of RAN email discussion about >6GHz channel modelling", Samsung.

[5] 3GPP TD R1-163408: "Additional Considerations on Building Penetration Loss Modelling for 5G System Performance Evaluation", Straight Path Communications.

[6] ICT-317669-METIS/D1.4: "METIS channel model, METIS 2020, Feb, 2015".

[7] Glassner, A S: "An introduction to ray tracing. Elsevier, 1989".

[8] McKown, J. W., Hamilton, R. L.: "Ray tracing as a design tool for radio networks, Network, IEEE, 1991(6): 27-30".

[9] Kurner, T., Cichon, D. J., Wiesbeck, W.: "Concepts and results for 3D digital terrain-based wave propagation models: An overview", IEEE J.Select. Areas Commun., vol. 11, pp. 1002–1012, 1993.

[10] Born, M., Wolf, E.: "Principles of optics: electromagnetic theory of propagation, interference and diffraction of light", CUP Archive, 2000.

[11] Friis, H.: "A note on a simple transmission formula", proc. IRE, vol. 34, no. 5, pp. 254–256, 1946.

[12] Kouyoumjian, R.G., Pathak, P.H.: "A uniform geometrical theory of diffraction for an edge in a perfectly conducting surface" Proc. IEEE, vol. 62, pp. 1448–1461, Nov. 1974.

[13] Pathak, P.H., Burnside, W., Marhefka, R.: "A Uniform GTD Analysis of the Diffraction of Electromagnetic Waves by a Smooth Convex Surface", IEEE Transactions on Antennas and Propagation, vol. 28, no. 5, pp. 631–642, 1980.

[14] IST-WINNER II Deliverable 1.1.2 v.1.2, "WINNER II Channel Models", IST-WINNER2, Tech. Rep., 2007 (<http://www.ist-winner.org/deliverables.html>).

[15] 3GPP TR36.101: "User Equipment (UE) radio transmission and reception".

[16] 3GPP TR36.104: "Base Station (BS) radio transmission and reception".

[17] Asplund, H., Medbo, J., Göransson, B., Karlsson, J., Sköld, J.: "A simplified approach to applying the 3GPP spatial channel model", in Proc. of PIMRC 2006.

[18] ITU-R Rec. P.1816: "The prediction of the time and the spatial profile for broadband land mobile services using UHF and SHF bands".

[19] ITU-R Rec. P.2040-1: "Effects of building materials and structures on radiowave propagation above about 100 MHz", International Telecommunication Union Radiocommunication Sector ITU-R, 07/2015.

[20] ITU-R Rec. P.527-3: "Electrical characteristics of the surface of the earth", International Telecommunication Union Radiocommunication Sector ITU-R, 03/1992.

[21] Jordan, E.C., Balmain, K.G.: "Electromagnetic Waves and Radiating Systems", Prentice-Hall Inc., 1968.

[22] 3GPP TD RP-162469: "Study on New Radio (NR) Access Technology".

[23] 3GPP TD RP-182138: "SID on Channel Modeling for Indoor Industrial Scenarios".

[26] 3GPP TD RP-242348: " Study on channel modelling for Integrated Sensing And Communication (ISAC) for NR ".

# 3 Definitions, symbols and abbreviations

## 3.1 Definitions

For the purposes of the present document, the terms and definitions given in TR 21.905 [1] apply.

## 3.2 Symbols

For the purposes of the present document, the following symbols apply:

 antenna radiation power pattern

 maximum attenuation

*d*2D 2D distance between Tx and Rx

*d*3D3D distance between Tx and Rx

 antenna element spacing in horizontal direction

 antenna element spacing in vertical direction

*f* frequency

*fc* center frequency /carrier frequency

*F*rx,u,θ Receive antenna element *u* field pattern in the direction of the spherical basis vector 

*F*rx,u,ϕ Receive antenna element *u* field pattern in the direction of the spherical basis vector 

*F*tx,s,θ Transmit antenna element *s* field pattern in the direction of the spherical basis vector 

*F*rx,s,ϕ Transmit antenna element *s* field pattern in the direction of the spherical basis vector 

*h*BS antenna height for BS

*h*UT antenna height for UT

 spherical unit vector of cluster *n*, ray *m*, for receiver

 spherical unit vector of cluster *n*, ray *m*, for transmitter

*α* bearing angle

*β* downtilt angle

*γ* slant angle

 wavelength

** cross-polarization power ratio in linear scale

**lgASA mean value of 10-base logarithm of azimuth angle spread of arrival

**lgASD mean value of 10-base logarithm of azimuth angle spread of departure

**lgDSmean value of 10-base logarithm of delay spread

**lgZSAmean value of 10-base logarithm of zenith angle spread of arrival

**lgZSDmean value of 10-base logarithm of zenith angle spread of departure

 LOS probability

 side-lobe attenuation in vertical direction

**lgASA standard deviation of 10-base logarithm of azimuth angle spread of arrival

**lgASD standard deviation of 10-base logarithm of azimuth angle spread of departure

**lgDSstandard deviation value of 10-base logarithm of delay spread

**lgZSA standard deviation of 10-base logarithm of zenith angle spread of arrival

**lgZSD standard deviation of 10-base logarithm of zenith angle spread of departure

 standard deviation of SF

 azimuth angle

 zenith angle

 spherical basis vector (unit vector) for GCS

 spherical basis vector (unit vector) for LCS

 horizontal 3 dB beamwidth of an antenna

 spherical basis vector (unit vector), orthogonal to , for GCS

 spherical basis vector (unit vector), orthogonal to , for LCS

 electrical steering angle in vertical direction

 vertical 3 dB beamwidth of an antenna

*ψ* Angular displacement between two pairs of unit vectors

## 3.3 Abbreviations

For the purposes of the present document, the abbreviations given in TR 21.905 [1] and the following apply. An abbreviation defined in the present document takes precedence over the definition of the same abbreviation, if any, in TR 21.905 [1].

2D two-dimensional

3D three-dimensional

AOA Azimuth angle Of Arrival

AOD Azimuth angle Of Departure

AS Angular Spread

ASA Azimuth angle Spread of Arrival

ASD Azimuth angle Spread of Departure

BF Beamforming

BS Base Station

BP Breakpoint

BW Beamwidth

CDF Cumulative Distribution Function

CDL Clustered Delay Line

CRS Common Reference Signal

D2D Device-to-Device

DFT Discrete Fourier Transform

DS Delay Spread

GCS Global Coordinate System

IID Independent and identically distributed

InF Indoor Factory

InF-SL Indoor Factory with Sparse clutter and Low base station height (both Tx and Rx are below the average height of the clutter)

InF-DL Indoor Factory with Dense clutter and Low base station height (both Tx and Rx are below the average height of the clutter)

InF-SH Indoor Factory with Sparse clutter and High base station height (Tx or Rx elevated above the clutter)

InF-DH Indoor Factory with Dense clutter and High base station height (Tx or Rx elevated above the clutter)

InF-HH Indoor Factory with High Tx and High Rx (both elevated above the clutter)

InH Indoor Hotspot

IRR Infrared Reflecting

ISD Intersite Distance

K Ricean K factor

LCS Local Coordinate System

LOS Line Of Sight

MIMO Multiple-Input-Multiple-Output

MPC Multipath Component

NLOS Non-LOS

O2I Outdoor-to-Indoor

O2O Outdoor-to-Outdoor

OFDM Orthogonal Frequency-Division Multiplexing

PAS Power angular spectrum

PL Path Loss

PRB Physical Resource Block

RCS Radar cross-section

RMa Rural Macro

RMS Root Mean Square

RSRP Reference Signal Received Power

Rx Receiver

SCM Spatial Channel Model

SINR Signal-to-Interference-plus-Noise Ratio

SIR Signal-to-Interference Ratio

SSCM Statistical Spatial Channel Model

SF Shadow Fading

SLA Sidelobe Attenuation

TDL Tapped Delay Line

TOA Time Of Arrival

TRP Transmission Reception Point

Tx Transmitter

UMa Urban Macro

UMi Urban Micro

UT User Terminal

UTD Uniform Theory of Diffraction

V2V Vehicle-to-Vehicle

XPR Cross-Polarization Ratio

ZOA Zenith angle Of Arrival

ZOD Zenith angle Of Departure

ZSA Zenith angle Spread of Arrival

ZSD Zenith angle Spread of Departure

# 4 Introduction

At TSG RAN #69 meeting the Study Item Description on "Study on channel model for frequency spectrum above 6 GHz" was approved [2]. This study item covers the identification of the status/expectation of existing information on high frequencies (e.g. spectrum allocation, scenarios of interest, measurements, etc), and the channel model(s) for frequencies up to 100 GHz. This technical report documents the channel model(s). The new channel model has to a large degree been aligned with earlier channel models for <6 GHz such as the 3D SCM model (TR 36.873) or IMT-Advanced (ITU-R M.2135). The new model supports comparisons across frequency bands over the range 0.5-100 GHz. The modelling methods defined in this technical report are generally applicable over the range 0.5-100 GHz, unless explicitly mentioned otherwise in this technical report for specific modelling method, involved parameters and/or scenario.

Subsequently, at the TSG RAN #81 meeting the Study Item Description "Study on Channel Modeling for Indoor Industrial Scenarios" was approved [23]. The findings from this study item is also captured in the present technical report. The Industrial channel model was developed by considering new measurements and information in the literature. An overview list of all such contributions and sources is available in tdoc R1-1909706.

At TSG RAN #102 meeting the Study Item Description “Study on channel modelling for Integrated Sensing And Communication (ISAC) for NR” was approved. The findings from this study item are captured in Clause 7.9.

The channel model is applicable for link and system level simulations in the following conditions:

- For system level simulations, supported scenarios are urban microcell street canyon, urban macrocell, indoor office, rural macrocell, and indoor factory.

- Bandwidth is supported up to 10% of the center frequency but no larger than 2GHz.

- Mobility of either one end of the link or both ends of the link is supported

- For the stochastic model, spatial consistency is supported by correlation of LSPs and SSPs as well as LOS/NLOS state.

- Large array support is based on far field assumption and stationary channel over the size of the array.

- The sensing target is assumed in the far field of the sensing transmitter/receiver for the channel model(s) for ISAC in Clause 7.9

# 5 Void

# 6 Status/expectation of existing information on high frequencies

**< Unchanged text omitted >**

# 7 Channel model(s) for 0.5-100 GHz

**< Unchanged text omitted >**

## 7.9 Channel model(s) for ISAC

### 7.9.0 Introduction

The channel model for ISAC in this clause is designed based on the channel model defined in the previous clauses within Clause 7 taking into account the known properties, e.g., location, Radar Cross-Section (RCS), polarization and etc. of one or more physical objects. A physical object is categorized as a sensing target (ST) or an environment object (EO). The large scale and small scale parameters of the channel between any two of sensing transmitter (STX), ST and sensing receiver (SRX) in a sensing scenario are obtained from the TRs[X] for the same communication scenario unless updates on the parameter values are specially described. The ST is considered as a receiver or transmitter, respectively, in the determination of a proper channel model for a STX-ST link or a ST-SRX link.

The common framework for the ISAC channel between a pair of STX and SRX is composed of a component for the target channel and a component for the background channel. A pair of STX and SRX can sense one or multiple STs. If blockage/forward scattering between sensing targets is not considered, a propagation path from Tx to Rx interacting with more than one sensing target is not modelled. The target channel of ST *k* includes all [multipath] components impacted by ST *k,* , where *K* is the number of STs. Such [multipath] components may interact with stochastic cluster(s) in either of or both the STX-ST link and ST-SRX link. The background channel includes other [multipath] components not belonging to the target channel.

### 7.9.1 Scenarios

The detailed sensing scenario description in this clause can be used for channel model calibration.

**ISAC-UAV**

Details on ISAC-UAV scenarios are listed in Table 7.9.1-1.

**Table 7.9.1-1: Evaluation parameters for UAV sensing scenarios**

|  |  |
| --- | --- |
| **Parameters** | **Value** |
| Applicable communication scenarios | UMi, UMa, RMa [38.901]UMi-AV, UMa-AV, RMa-AV |
| Sensing transmitters and receivers properties | Rx/Tx Locations | Rx/Tx locations are selected among the TRPs and UEs locations in the corresponding communication scenarios.NOTE1: This may include aerial UEs for UMi-AV, UMa-AV, RMa-AV communication scenarios. In this case, other Rx/Tx properties (e.g. mobility) are also taken from the corresponding communication scenario. |
| Sensing target | LOS/NLOS | LOS and NLOS  |
| Outdoor/indoor | Outdoor |
| 3D mobility | Horizontal velocity: uniform distribution between 0 and 180km/h, if horizontal velocity is not fixed to 0. Vertical velocity: 0km/h, optional {20, 40} km/hNOTE2: 3D mobility can be horizontal only or vertical only or a combination for each sensing targetNOTE 3: time-varying velocity may be considered for future evaluations. |
| 3D distribution | Horizontal plane: Option A: *N* targets uniformly distributed within one cell. Option B: *N* targets uniformly distributed per cell. Option C: *N* targets uniformly distributed within an area not necessarily determined by cell boundaries.*N* = {1, 2, 3, 4, 5}NOTE4: *N*=0 may be considered for the evaluation of false alarmVertical plane: Option A: Uniform between 1.5m and 300m.Option B: Fixed height value chosen from {25, 50, 100, 200, 300} m assuming vertical velocity is equal to 0.  |
| Orientation | Random in horizontal domain |
| Physical characteristics (e.g., size) | Size:* Option 1: 1.6m x 1.5m x 0.7m
* Option 2: 0.3m x 0.4m x 0.2m
 |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | Min distances based on min. TRP/UE distances defined in TR36.777 as a starting point.NOTE5: the sensing target is assumed in the far field of sensing Tx/Rx |
| Minimum 3D distance between sensing targets | Option 1: At least larger than the physical size of a targetOption 2: 10 meters |
| [Unintended/Environment objects, e.g., types, characteristics, mobility, distribution, etc.] | FFS |

NOTE: A percentage of TRPs/UEs that have sensing capabilities may be considered for future evaluations.

**ISAC-Automotive**

Details on ISAC-Automotive scenarios are listed in Table 7.9.1-2.

**Table 7.9.1-2: Evaluation parameters for Automotive sensing scenarios**

|  |  |
| --- | --- |
| **Parameters** | **Values** |
| Applicable communication scenarios | Highway, Urban Grid. NOTE1 |
| Sensing transmitters and receivers properties | Rx/Tx locations are selected among the TRPs and UEs (e.g., VRU, vehicle, RSU-type UEs) locations in the corresponding communication scenario. NOTE2Additional option: ISD between TRPs of Urban Grid is 250m |
| Sensing target | LOS/NLOS | LOS and NLOS (including NLOSv) |
| Outdoor/indoor | Outdoor |
| Mobility (horizontal plane only) | Based on TR37.885 mobility for urban grid or highway scenario |
| Distribution (horizontal) | Based on dropping in TR37.885 per urban grid or highway communication scenario  |
| Orientation | Lane direction in horizontal plane |
| Physical characteristics (e.g., size) | Type 1/2 (passenger vehicle) Type 3 (truck/bus) Vehicle type distribution per TR 37.885 as a starting point |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | Min distances based on min. TRP/UE distances defined in TR37.885 as a starting point.NOTE3: the sensing target is assumed in the far field of sensing Tx/Rx |
| Minimum 3D distance between sensing targets | Option 1: At least larger than the physical size of a sensing targetOption 2: Fixed value, 10 m.  |
| Environment Objects, e.g., types, characteristics, mobility, distribution, etc. | EO Type 2 for Urban Grid* up to 4 walls modelled as EO type 2, per building of size 413m x 230m x 20m. FFS: number of buildings, how many walls are modelled, additional building sizes, etc.
 |

NOTE1: calibration for UMi, Uma, RMa is not performed for the automotive scenario, but UMi, Uma, RMa can be considered for future evaluations of the automotive sensing target scenarios. Calibration for UMi, Uma, RMa is expected to be performed for another sensing scenario.

NOTE2: A percentage of TRPs/UEs that have sensing capabilities may be considered for future evaluations.

**ISAC-Human**

Details on ISAC-Human scenarios are listed in Table 7.9.1-3.

**Table 7.9.1-3: Evaluation parameters for Human (indoor and outdoor) sensing scenarios**

|  |  |  |
| --- | --- | --- |
| **Parameters** | **Indoor Values** | **Outdoor Values** |
| Applicable communication scenarios NOTE1 | Indoor office, indoor factory [TR38.901]Indoor room [TR38.808] | UMi, Uma, RMa [TR38.901] |
| Sensing transmitters and receivers properties | Rx/Tx LocationsNOTE 2 | Rx/Tx locations are selected among the TRPs and UE locations in the corresponding communication scenario | Rx/Tx locations are selected among the TRPs and UE locations in the corresponding communication scenario |
| Rx/Tx Mobility for UEs | Option 1: 0km/hOption 2: 3km/hOption 3: Uniform distribution between 0km/h and 3km/hr | Option 1: 0km/hOption 2: 3km/hOption 3: Uniform distribution between 0km/h and 10km/hr |
| Sensing target | LOS/NLOS | LOS and NLOS  | LOS and NLOS |
| Outdoor/indoor | Indoor | Outdoor |
| 3D mobility | Option 1: 0km/hOption 2: 3km/hOption 3: Uniform distribution between 0km/h and 3km/hr (horizontal plane with random direction straight-line trajectory) | Option 1: 0km/hOption 2: 3km/hOption 3: Uniform distribution between 0km/h and 10km/hr (horizontal plane with random direction straight-line trajectory) |
| 3D distribution | *N* targets uniformly distributed over the horizontal area of the convex hull of the TRP deploymentNOTE1: *N*=0 may be considered for the evaluation of false alarm | Option A: *N* targets uniformly distributed within one cell. Option B: *N* targets uniformly distributed per cell. Option C: *N* targets uniformly distributed within an area not necessarily determined by cell boundaries. NOTE1: *N*=0 may be considered for the evaluation of false alarm |
| Orientation | Random over the horizontal area | Random over the horizontal area |
| Physical characteristics (e.g., size) | Size (Length x Width x Height):* Child: 0.2m x 0.3m x 1m
* Adult Pedestrian: 0.5m x 0.5m x 1.75m
 | Size (Length x Width x Height):* Child: 0.2m x 0.3m x 1m
* Adult Pedestrian: 0.5m x 0.5m x 1.75m
 |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | Min distances defined in TR 38.901 and TR36.843 and TR38.859as a starting pointNOTE2: the sensing target is assumed in the far field of sensing Tx/Rx | Min distances defined in TR 38.901 and TR36.843 and TR38.859 as a starting pointNOTE3: the sensing target is assumed in the far field of sensing Tx/Rx |
| Minimum 3D distance between sensing targets | Option 1: At least larger than the physical size of a sensing targetOption 2: Fixed value, [x] m. value of x is FFS | Option 1: At least larger than the physical size of a sensing targetOption 2: Fixed value, [x] m. value of x is FFS |
| Environment Objects, e.g., types, characteristics, mobility, distribution, etc. | FFS, based on outcome for AI 9.7.2 | FFS, based on outcome for AI 9.7.2 |

NOTE1: For the human (indoor and outdoor) sensing targets, additional communication scenarios can be considered for future evaluations. Channel model calibration for Urban Grid with outdoor humans is expected to be performed from Objects creating hazards on the road/railway sensing scenarios.

NOTE2: A percentage of TRPs/UEs that have sensing capabilities may be considered for future evaluations.

**ISAC-AGV**

Details on ISAC-AGV are listed in Table 7.9.1-4.

**Table 7.9.1-4: Evaluation parameters for Automated Guided Vehicles**

|  |  |
| --- | --- |
| **Parameters** | **Value** |
| Applicable communication scenarios NOTE1 | InF (TR38.901 including Table 7.8-7) |
| Sensing transmitters and receivers properties NOTE2 | Rx/Tx location are selected among the TRPs and UEs location in the corresponding communication scenarioRx/Tx Mobility for UEs* Option 1: 0 km/h
* Option 2: 3km/h
* Option 3: Uniform distribution between 0km/h and 3km/h
 |
| Sensing target | LOS/NLOS | LOS and NLOS |
| Outdoor/indoor | Indoor |
| 3D mobility | Horizontal velocity with random straight-line trajectory * Option 1: Uniform distribution in the range of up to 30 km/h
* Option 2: Fixed velocities [3, 10] km/h
 |
| 3D distribution | Option A: Uniformly distributed in the convex hull of the horizontal BS deploymentOption B: Uniformly distributed in horizontal plane |
| Orientation | Horizontal plane only |
| Physical characteristics (e.g., size) | Size (L x W x H)* Option 1: 0.5m x 1.0m x 0.5m
* Option 2: 1.5 m x 3.0m x 1.5 m
* FFS: Material, Additional sizes, and AGV size distribution
 |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | Min distances based on min. TRP/UE distances defined in TR38.901NOTE: the sensing target is assumed in the far field of sensing Tx/Rx |
| Minimum 3D distance between sensing targets | Option A: At least larger than the physical size of a targetOption B: Fixed value, [x] m. value of x is FFS |
| Environment objects, e.g., types, characteristics, mobility, distribution, etc. | FFS |

NOTE1: For the AGV sensing targets, additional communication scenarios can be considered for future evaluations.

NOTE2: A percentage of TRPs/UEs that have sensing capabilities may be considered for future evaluations.

NOTE3: RAN1 can further discuss narrowing down the number of sub-scenarios of InF

**ISAC-Objects creating hazards**

Details on ISAC-Hazards are listed in Table 7.9.1-5.

**Table 7.9.1-5: Evaluation parameters for objects creating hazards**

|  |  |
| --- | --- |
| **Parameters** | **Value** |
| Applicable communication scenarios NOTE1 | Highway, Urban grid, HST (High Speed Train) |
| Sensing transmitters and receivers propertiesNOTE2 | Rx/Tx Locations | Rx/Tx locations are selected among the TRPs and UEs (e.g., VRU, vehicle, RSU-type UEs) locations in the corresponding communication scenarios.Additional option ISD between TRPs of Urban Grid is 250 m |
| Sensing target | LOS/NLOS | LOS and NLOS |
| Outdoor/indoor | Outdoor |
| 3D mobility | Horizontal velocity: up to [10] km/h for humans and animalsFFS: Additional velocities, trajectory |
| 3D distribution | Uniformly distributed in horizontal plane |
| Orientation | Random distribution in horizontal plane |
| Physical characteristics (e.g., size) | For human/pedestrians: Child: 0.2m x 0.3m x 1mAdult: 0.5m x 0.5m x 1.75m For animals:Size: 1.5m x 0.5m x 1 m |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | Min. distance is based onmin TRP/UE distances defined in TR37.885 and TR38.802 and TR36.843 and TR38.859NOTE: the sensing target is assumed in the far field of sensing Tx/Rx |
| Minimum 3D distance between sensing targets | Option 1: At least larger than the physical size of a sensing targetOption 2: Fixed value, 10 m.  |
| Environment objects, e.g., types, characteristics, mobility, distribution, etc. | EO Type 2 for Urban Grid* up to 4 walls modelled as EO type 2, per building of size 413m x 230m x 20m. FFS: number of buildings, how many walls are modelled, additional building sizes, etc.
 |

NOTE1: For the objects creating hazards sensing targets, additional communication scenarios can be considered for future evaluations.

NOTE2: A percentage of TRPs/UEs that have sensing capabilities may be considered for future evaluations.

### 7.9.2 Physical object model

#### 7.9.2.0 Introduction

A ST is an object of interest for sensing. An EO is a non-target object with known location. Two types of EO are supported in the ISAC channel model. A first type of EO (type-1 EO) has similar characteristic as a ST and is modelled in the same way as a ST. A second type of EO (type-2 EO, 7.9.5.2) is of large size and is modelled differently from a ST.

In the following descriptions in Clause 7.9, only the related details on ST are described, which is also applicable to type-1 EO.

A ST is modelled with one or multiple scattering points. Each scattering point of a ST (SPST) is used to model the total scattering effects of some adjacent scattering centres at the ST. The impact of a SPST to the channel is modelled from two aspects, i.e., the RCS (Radar Cross Section, 7.9.2.1) and the polarization matrix (7.9.2.2). The RCS of the SPST is a scalar value and is defined as the hypothetical area required to intercept the incident power at the SPST such that if the total intercepted power were re-radiated, the power density actually observed at the receiver would be produced. The polarization matrix of the SPST includes the effect of phase and amplitude of co-polarization and cross-polarization at the SPST. The polarization matrix of the SPST is separately modelled from other polarization effects introduced by stochastic clusters and/or EOs in the target channel.

#### 7.9.2.1 RCS of a sensing target

The RCS of a SPST is dependent on both the incident angle and the scattered angle. A subset of the RCS values with same incident/scattered angles can be referred as monostatic RCS values.

The RCS related coefficient of a SPST for a pair of incident/scattered angles is composed of a first component which is included in the large-scale parameters, and a second component and third component which are both included in the small-scale parameters, i.e., . is deterministic value for the SPST. can be fixed to 1 or can be angular dependent. follows log-normal distribution. The mean and standard deviation used to characterize satisfied a fixed relation . is separately determined for each pair of incident/scattered angels at the SPST. [correlation]

A first RCS model is to characterize a ST as single SPST with component of the monostatic RCS values fixed to 1. is the mean of linear monostatic RCS values at the SPST. The logarithmic values of of the monostatic RCS values for the sensing targets are provided in Table 7.9.2.1-1.

**Table 7.9.2.1-1: Parameters on RCS for the targets with angular independent monostatic RCS values**

|  |  |  |  |
| --- | --- | --- | --- |
| **Sensing target** | **(dBsm)** | **(dB)** | **(dB)** |
| UAV of small size | -12.81  | 0  | 3.74  |
| Human with RCS model 1 | -1.37  | 0  | 3.94  |

A second RCS model is to split a ST into single or multiple SPSTs, and adopts an angular dependent component of the monostatic RCS values for each SPST. For UAV with large size and human, single SPST is modelled. While for vehicle [and AGV], both models with single and multiple SPSTs are provided. For vehicle modelled with multiple scattering points, the recommended five scattering points are located at the front, left, back, right and roof side of the vehicle respectively. The orientation of a sensing target in LCS is provided as follows.

* The front of a vehicle, a UAV with large size or an AGV has azimuth angle and zenith angle in LCS.
* For a human, it faces the direction of azimuth angle and zenith angle in LCS.

For UAV of large size with single scattering point, human with RCS model 2, and AGV with single[/multiple SPSTs], the values/pattern , denoted as , of the monostatic RCS values for a SPST is deterministic based on incident/scattered angles

Where,

The parameters to define of the monostatic RCS values for the sensing targets are provided in Table 7.9.2.1-2/3/6/7.

For vehicle with single/multiple SPSTs, the values/pattern , denoted as , of the RCS for a SPST is deterministic based on the incident angle () and the scattered angle ().

With defined by,

Where,

* + () are the bisector angle between incident angle () and scattered angle (), i.e., .
	+ . is the bistatic angle between the incident ray and scattering ray within the plane defined by incident angle () and scattering angle ().
		- for vehicle
	+ is for the effect of forward scattering and is set to

For a vehicle with single scattering point, sets of parameters , *Range of* and *Range of* are defined. The bisector angle () is used to index one set from the sets of parameters, and determine of the vehicle consequently. If the vehicle is split into scattering points, with each scattering point characterized by one of sets of parameters, are respectively determined for each scattering point.

The sets of parameters to define and the parameters of the RCS for the vehicle are provided in Table 7.9.2.1-4/5.

**Table 7.9.2.1-2: Parameters on RCS for UAV with large size**

|  |  |  |  |
| --- | --- | --- | --- |
|  |  **(dBsm)** | **(dBsm)** | **(dB)** |
| **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  |  | ***Range of*  in [**°**]** | ***Range of*  in [**°**]** |
| Left | 90 | 7.13 | 90 | 8.68 | 7.43 | 14.30 | [45,135] | [45,135] | [] | 2.50 |
| Back | 180 | 10.09 | 90 | 11.43 | 3.99 | 10.86 | [45,135] | [135,225] |
| Right | 270 | 7.13 | 90 | 8.68 | 7.43 | 14.30 | [45,135] | [225,315] |
| Front | 0 | 14.19 | 90 | 16.53 | 1.02 | 7.89 | [45,135] | [-45,45] |
| Bottom | / | / | 180 | 4.93 | 13.55 | 20.42 | [135,180] | [0,360] |
| Roof | / | / | 0 | 4.93 | 13.55 | 20.42 | [0,45] | [0,360] |

Note: When is in the range [0,45] or [135,180], .

**Table 7.9.2.1-3: Parameters on RCS for human with RCS model 2**

|  |  |  |  |
| --- | --- | --- | --- |
|  |  **(dBsm)** | **(dBsm)** | **(dB)** |
| **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  |  | ***Range of*  in [**°**]** | ***Range of*  in [**°**]** |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

**Table 7.9.2.1-4: Parameters on RCS for vehicle with single scattering point**

|  |  |  |  |
| --- | --- | --- | --- |
|  |  **(dBsm)** | **(dBsm)** | **(dB)** |
| **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  |  | ***Range of*  in [**°**]** | ***Range of*  in [**°**]** |
| Left | 90 | 26.90  | 79.70  | 44.42  | 20.75  | 13.68  | [30,180] | (45,135] | **[]** | 3.41 |
| Back | 180 | 36.32  | 79.65  | 36.73  | 14.56  | 7.50  | [30,180] | (135,225] |
| Right | 270 | 26.90  | 79.70  | 44.42  | 20.75  | 13.68  | [30,180] | (225,315] |
| Front | 0 | 40.54  | 71.75  | 29.13  | 15.52  | 8.45  | [30,180] | (-45, 45] |
| Roof | - | - | 0.00  | 18.13  | 21.26  | 14.19  | [0,30) | [0,360) |

Note: When is in the range [0, 30), .

**Table 7.9.2.1-5: Parameters on RCS for vehicle with multiple scattering points**

|  |  |  |  |
| --- | --- | --- | --- |
|  |  **(dBsm)** | **(dBsm)** | **(dB)** |
| **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  |  | ***Range of*  in [**°**]** | ***Range of*  in [**°**]** |
| Left | 90 | 26.90 | 79.70 | 44.42 | 20.60 | 20.52 | [0,180] | [0,360] | **[]** | 3.41 |
| Back | 180 | 36.32 | 79.65 | 36.73 | 13.90 | 13.82 | [0,180] | [0,360] |
| Right | 270 | 26.90 | 79.70 | 44.42 | 20.60 | 20.52 | [0,180] | [0,360] |
| Front | 0 | 40.54 | 71.75 | 29.13 | 14.99 | 14.91 | [0,180] | [0,360] |
| Roof | - | - | 0.00 | 18.13 | 21.12 | 21.05 | [0,180] | [0,360] |

Note: For the scattering point associated with roof of the vehicle, .

**Table 7.9.2.1-6: Parameters on RCS for AGV with single scattering point**

|  |  |  |  |
| --- | --- | --- | --- |
|  |  **(dBsm)** | **(dBsm)** | **(dB)** |
| **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  |  | ***Range of*  in [**°**]** | ***Range of*  in [**°**]** |
| Front | 0 | 13.68 | 90 | 13.68 | 13.02  | 23.29  | [30,180] | [45,135] | [] | 2.51 |
| Left | 90 | 15.53 | 75 | 20.03 | 7.33  | 17.60  | [30,180] | [135,225] |
| Back | 180 | 12.49 | 90 | 11.89 | 11.01  | 21.28  | [30,180] | [225,315] |
| Right | 270 | 15.53 | 75 | 20.03 | 7.33  | 17.60  | [30,180] | [-45,45] |
| Roof | / | / | 0 | 11.44 | 11.79  | 22.06  | [0,30] | [0,360] |

Note: When is in the range [0,30), .

**[Table 7.9.2.1-7: Parameters on RCS for AGV with multiple scattering points]**

|  |  |  |  |
| --- | --- | --- | --- |
|  |  **(dBsm)** | **(dBsm)** | **(dB)** |
| **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  **in [**°**]** |  |  | ***Range of*  in [**°**]** | ***Range of*  in [**°**]** |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

#### 7.9.2.2 Cross-polarization matrix of a sensing target

The cross-polarization matrixof a SPST for a pair of incident/scattered angles is generally modelled by amplitude factors and initial random phases , i.e.,

 (7.9-xx)

For UAV, human, vehicle or AGV, , , i.e.,

 (7.9-xx)

where,

* is the XPR of the pair of incident/scattered angles. is randomly generated by log-normal distribution per target type defined in Table 7.9.2.2-1.
* is uniformly distributed within

**Table 7.9.2.2-1: Parameters on XPR (dB) for the targets**

|  |  |  |
| --- | --- | --- |
| **Target** | ****XPR** | ****XPR** |
| UAV | 13.75 | 7.07 |
| Human | 19.81 | 4.25 |
| Vehicle  | 21.12 | 6.88 |
| AGV | [] | [] |

### 7.9.3 Reference channel models and required updates

A transmitter or receiver in the sensing operation can be TRP, terrestrial UE, vehicle UE, aerial UE, AGV UE or RSU-type UE. The reference TR(s) for each combination of transmitter and receiver for each sensing scenario are provided in Table 7.9.3-1, where the terrestrial UE, AGV and RSU-type UE are referred as terrestrial UE.

**Table 7.9.3-1: Reference TRs to generate channel for ISAC**

|  |  |  |  |
| --- | --- | --- | --- |
| **Case** | **Tx/Rx** | **Rx/Tx** | **Reference TR to define the channel model** |
| 1 | TRP  | TRP | For sensing scenario UMi, UMa, RMa, InH, InF, UMi-AV, UMa-AV, and RMa-AV:* TRP-TRP link of scenario UMi, UMa, InH, and InF following the option based on TR 38.901 defined in Clause A.3 of TR 38.858
	+ For InF, hUE is changed to the same height as the BS
* TRP-UE link of scenario RMa defined in Clause 7 of TR 38.901 by setting hUE=35m (NOTE 1)

For sensing scenario Highway * TRP-UE link of scenario RMa in section 7 of TR 38.901 by setting hUE=35m for FR1(NOTE 1)
* TRP-TRP link of scenario UMa following the option based on TR 38.901 defined in section A.3 of TR 38.858

For sensing scenario Urban grid* TRP-TRP link of scenario UMa following the option based on TR 38.901 defined in section A.3 of TR 38.858

For sensing scenario HST* TRP-UE link of scenario RMa in section 7 of TR 38.901 by setting hUE=35m for FR1 (NOTE 1)
* TRP-TRP link of scenario UMa following the option based on TR 38.901 defined in section A.3 of TR 38.858 for FR2
 |
| 2 | TRP  | terrestrial UE | For sensing scenario UMi, UMa, RMa, InH, InF, UMi-AV, UMa-AV, and RMa-AV* TRP-UE link of scenario UMi, UMa, RMa, InH, and InF in Clause 7 of TR 38.901

For sensing scenario Highway and Urban grid* P2B link of scenario Highway and Urban grid in Clause 6 of TR 37.885

For sensing scenario HST* TRP-UE link of scenario RMa in Clause 7 of TR 38.901 for FR1 and TRP-UE link of scenario UMa in Clause 7 of TR 38.901 for FR2
 |
| 3 | TRP  | vehicle UE | For sensing scenario Highway and Urban grid * V2B link of scenario Highway and Urban grid in Clause 6 of TR 37.885

For sensing scenario UMi, UMa, and RMa* TRP-UE link of scenario UMi, UMa, and RMa in Clause 7 of TR 38.901
 |
| 4 | TRP  | aerial UE | For sensing scenario UMa-AV, UMi-AV, and RMa-AV * TRP-aerial UE link of scenario UMa-AV, UMi-AV, and RMa-AV in Clause Annex A and B of TR 36.777 for FR1
* Reuse the channel model of scenario UMa-AV, UMi-AV, and RMa-AV of FR1 for FR2
 |
| 5 | terrestrial UE | terrestrial UE | For sensing scenario UMi, UMa, RMa, InH, InF, UMi-AV, UMa-AV, and RMa-AV:* UE-UE link of scenario UMi, UMa, InH, and InF following the option based on TR 38.901 defined in Clause A.3 of TR 38.858
* TRP-UE link of scenario RMa defined in Clause 7 of TR 38.901 by setting hBS =1.5m (NOTE 2)

For sensing scenario Highway and Urban grid* For pedestrian type UE:
	+ P2P link in section 6 of TR 37.885

For sensing scenario HST* TRP-UE link of scenario RMa in section 7 of TR 38.901 for FR1, e.g., hBS=1.5m, UE-UE link of scenario UMa following the option based on TR 38.901 defined in section A.3 of TR 38.858 for FR2
 |
| 6 | terrestrial UE | vehicle UE | For sensing scenario UMi, UMa, RMa* UE-UE link of scenario UMi, UMa following the option based on TR 38.901 defined in section A.3 of TR 38.858
* TRP-UE link of scenario RMa defined in section 7 of TR 38.901 by setting hBS =1.5m

For sensing scenario Highway and Urban grid* For pedestrian type UE:
	+ V2P link in section 6 of TR 37.885
 |
| 7 | terrestrial UE | aerial UE | For sensing scenario UMi-AV, UMa-AV, and RMa-AV* TRP-aerial UE link of UMi-AV in Annex A and B of TR 36.777 by setting hBS =1.5m for FR1
	+ LOS probability is not reused, FFS new LOS probability
	+ FFS pathloss model, shadowing fading
* Reuse the channel model of scenario UMa-AV, UMi-AV, and RMa-AV of FR1 for FR2
	+ The corresponding parameter values in FR2 are used
 |
| 8 | vehicle UE | vehicle UE | For sensing scenario Highway and Urban grid * V2V link of scenario Highway and Urban grid in section 6 of TR 37.885

For sensing scenario UMi, UMa, and RMa* UE-UE link of scenario UMi, UMa following the option based on TR 38.901 defined in section A.3 of TR 38.858
* TRP-UE link of scenario RMa defined in section 7 of TR 38.901 by setting hBS =1.5m
 |
| 9 | aerial UE | aerial UE | For sensing scenario UMi-AV, UMa-AV, RMa-AV* TRP-aerial UE link of UMi-AV in Annex A and B of TR 36.777 by setting height of TRP equal to the height of the first aerial UE for FR1
	+ LOS probability is not reused, FFS new LOS probability
	+ FFS pathloss model, shadowing fading, angular spread
* Reuse the channel model of scenario UMa-AV, UMi-AV, and RMa-AV of FR1 for FR2
	+ The corresponding parameter values in FR2 are used
 |

NOTE 1: ASA and ZSA statistics updated to be the same as ASD and ZSD; ZoD offset = 0

NOTE 2: ASD and ZSD statistics updated to be the same as ASA and ZSA.

The large scale and small scale parameters of the STX-ST link and the ST-SRX link for a sensing scenario are determined according to Table 7.9.3-1 assuming the same sensing scenario. The targets of UAV, vehicle are respectively considered as an aerial UE, vehicle UE. Other targets are considered as terrestrial UE. The proper case for each combination of STX/STX and ST are provided in Table 7.9.3-2.

**Table 7.9.3-2: Channel model for STX-ST and ST-SRX link**

|  |  |  |
| --- | --- | --- |
| **STX/SRX** | **Target** | **Cases in Table 7.9.3-1 assuming the same sensing scenario** |
| TRP | UAV | Case 4: TRP-Aerial UE link  |
| Human | Case 2: TRP-normal UE link  |
| Vehicle | Case 3: TRP-Vehicle UE link  |
| AGV | Case 2: TRP-normal UE link  |
| Object (Hazard) | Case 2: TRP-normal UE link  |
| Terrestrial UE | UAV | Case 7: normal UE - Aerial UE link  |
| Human | Case 5: normal UE-normal UE link  |
| Vehicle | Case 6: normal UE - Vehicle UE link  |
| AGV | Case 5: normal UE-normal UE link  |
| Object (Hazard) | Case 5: normal UE-normal UE link  |
| Vehicle UE | Human | Case 6: normal UE - Vehicle UE link  |
| Vehicle | Case 8: Vehicle UE - Vehicle UE link  |
| Object (Hazard) | Case 6: normal UE - Vehicle UE link  |
| Aerial UE | UAV | Case 9: Aerial UE - Aerial UE link  |
| AGV UE | AGV | Case 5: normal UE - normal UE link  |

The large scale and small scale parameters of the STX-SRX link, i.e., background channel for a sensing scenario are determined according to Table 7.9-1 assuming the same sensing scenario. The proper case for each combination of STX and SRX are provided in Table 7.9-3.

**Table 7.9.3-3: Channel model for background channel**

|  |  |  |
| --- | --- | --- |
| **STX/SRX** | **SRX/STX** | **Cases in Table 7.9.3-1 assuming the same sensing scenario** |
| TRP | TRP | Case 1: TRP-TRP link |
| Terrestrial UE | Case 2: TRP-normal UE link |
| Vehicle UE | Case 3: TRP-Vehicle UE link |
| Aerial UE | Case 4: TRP-Aerial UE link |
| AGV UE | Case 2: TRP-normal UE link |
| Terrestrial UE | Terrestrial UE | Case 5: normal UE-normal UE link |
| Vehicle UE | Case 6: normal UE - Vehicle UE link |
| Aerial UE | Case 7: normal UE - Aerial UE link |
| AGV UE | Case 5: normal UE -normal UE link |
| Vehicle UE | Vehicle UE | Case 8: Vehicle UE - Vehicle UE link |
| Aerial UE | Aerial UE | Case 9: Aerial UE - Aerial UE link |
| AGV UE | AGV UE | Case 5: normal UE - normal UE link |

The following updates to the reference TRs are identified to generate ISAC channel.

* For human as a sensing target with a single scattering point, the height of the scattering point is 1.5 m.
* For sensing scenario UMi, UMa, RMa, UMi-AV, UMa-AV and RMa-AV, the height of a scattering point of a target is used to calculate the LOS probability and pathloss, regardless of the lower bound of hUT in the reference TRs that are used to generate ISAC channel.

### 7.9.4 Fast fading model

#### 7.9.4.0 Introduction

A stepwise procedure illustrated in Figure 7.9.4-1 is used to generated the channel model for ISAC referring to the procedure in Clause 7.5 with parameters derived by Table 7.9.3-2 and 7.9.3-3. Step 1 is commonly executed, followed by the respective steps for target channel (7.9.4.1) and background channel (7.9.4.2). Finally, the target channel and background channel are combined to form the final channel model for ISAC (7.9.4.3).



Figure 7.9.4-1 Channel coefficient generation procedure

Step 1: Set environment, network layout, and antenna array parameters

a) Choose one of the sensing scenarios (ISAC-UAV, ISAC-Automative, ISAC-Human, ISAC-AGV, ISAC-Objects creating hazardsHaz) and related communication scenarios (e.g. UMa, UMi-Street Canyon, RMa, InH-Office, Urban grid, Highway, or InF). Choose a global coordinate system and define zenith angle *θ*, azimuth angle *ϕ*, and spherical basis vectors , as shown in Figure 7.5-2. Note: Scenario RMa is for up to 7GHz while others are for up to 100GHz.

b) Give number of STX, ST and SRX. Give the number of the SPST(s) of each ST.

c) Give 3D locations of STX and SRX, give 3D locations of SPST(s) of each ST, and determine LOS AOD (*ϕLOS,AOD*), LOS ZOD (*θLOS,ZOD*), LOS AOA (*ϕLOS,AOA*), and LOS ZOA (*θLOS,ZOA*) of each pair of STX and SPST, and each pair of SPST and SRX in the global coordinate system

d) Give STX and SRX antenna field patterns *Frx* and *Ftx* in the global coordinate system and array geometries.

e) Give STX and SRX array orientations with respect to the global coordinate system. STX array orientation is defined by three angles Ω*STX,α* (STX bearing angle), Ω*STX,β* (STX downtilt angle) and Ω*STX,γ* (STX slant angle). SRX array orientation is defined by three angles Ω*SRX,α* (SRX bearing angle), Ω*SRX,β* (SRX downtilt angle) and Ω*SRX,γ* (SRX slant angle). Give the orientation of ST in the global coordinate system. ST orientation is defined by three angles Ω*ST,α* (ST bearing angle), Ω*ST,β* (ST downtilt angle) and Ω*ST,γ* (ST slant angle).

f) Give speed and direction of motion of STX, ST and SRX in the global coordinate system

g) Specify system centre frequency and bandwidth

Note: In case wrapping is used, each wrapping copy of a STX or SRX should be treated as a separate STX/SRX considering channel generation.

For monostatic sensing mode, a STX and a corresponding SRX have the same 3D locations, antenna field pattern, array orientations, speed and direction of motion.

#### 7.9.4.1 Target channel

Following Step 1 in Clause 7.9.4.0, the target channels for the one or multiple STs between a pair of STX and SRX is generated using the following procedure with parameters derived by Table 7.9.3-2. It assumes a ST *k* consists of *P* scattering points, .

**Large scale parameters:**

Step 2: Assign propagation condition (LOS/NLOS) for each pair of STX and SPST, and each pair of SPST and SRX according to Table 7.4.2-1 updated as necessary in Clause 7.9.3..

Step 3: Calculate pathloss with formulas in Table 7.4.1-1 updated as necessary in Clause 7.9.3 for each STX-SPST link, and each SPST-SRX link.

Step 4: For each STX-SPST link and SPST-SRX link, generate large scale parameters, e.g. delay spread (DS), angular spreads (ASA, ASD, ZSA, ZSD), Ricean K factor (K) and shadow fading (SF) taking into account cross correlation according to Table 7.5-6 and using the procedure described in clause 3.3.1 of [14] with the square root matrix being generated using the Cholesky decomposition and the following order of the large scale parameter vector: **s***M* = [*sSF, sK, sDS, sASD, sASA, sZSD, sZSA*]*T*.

The LSPs for links from co-sited sectors to a STX/SPST/SRX are the same. In addition, these LSPs for the links of STX/SPST/SRX on different floors are uncorrelated.

Limit random RMS azimuth arrival and azimuth departure spread values to 104 degrees, i.e., ASA= min(ASA, 104°), ASD= min(ASD, 104°). Limit random RMS zenith arrival and zenith departure spread values to 52 degrees, i.e., ZSA= min(ZSA, 52°), ZSD= min(ZSD, 52°).

For monostatic sensing mode, the large scale parameters generated in step 2-4 are identical for a STX-SPST link and the corresponding SPST-SRX link of same SPST.

**Small scale parameters:**

Step 5: Generate cluster delays

The cluster delays of cluster n in a STX-SPST link are generated using Step 5 of Clause 7.5, i.e.,.

The cluster delays of cluster in the corresponding SPST-SRX link of same SPST are generated using Step 5 of Clause 7.5 by replacing subscript *n* with *n’*, i.e., .

Step 6: Generate cluster powers.

The cluster power of cluster n in a STX-SPST link are generated using Step 6 fo Clause 7.5, i.e., .

The cluster power of cluster in the corresponding SPST-SRX link of same SPST are generated using Step 6 of Clause 7.5 by replacing subscript *n* with *n’*, i.e., .

Step 7: Generate arrival angles and departure angles for both azimuth and elevation.

The arrival angles and departure angles for both azimuth and elevation of a cluster *n* in a STX-SPST link are generated using Step 7 of Clause 7.5, i.e., , , , .

The arrival angles and departure angles for both azimuth and elevation of a cluster *n’* in the corresponding SPST-SRX link of same SPST are generated using Step 7 of Clause 7.5 by replacing subscript *n, m* with *n’, m’*, i.e.,, , , .

For monostatic sensing mode, are respectively equal to in Step 5-7, if and if applicable .

Step 8: Coupling of rays within a cluster for both azimuth and elevation.

The rays within a cluster *n* for both azimuth and elevation in a STX-SPST link are coupled using Step 8 of Clause 7.5.

The rays within a cluster *n’* for both azimuth and elevation in the corresponding SPST-SRX link of same SPST are coupled using Step 8 of Clause 7.5 by replacing subscript *n, m* with *n’, m’*.

For monostatic sensing mode, the same ray-coupling way apples to both the STX-SPST link and the SPST-SRX link.

Step 9: Coupling of rays for a STX-SPST link and the corresponding SPST-SRX link of same SPST.

In the STX-SPST link, a LOS ray is represented by , while a NLOS ray *m* of a stochastic cluster *n* is represented by . In the SPST-SRX link, a LOS ray is represented by while a NLOS ray *m’* of a stochastic cluster *n’* is represented by . A ray in the STX-SPST link and a ray in the corresponding SPST-SRX link that are coupled to each other construct a path

The LOS ray (if present) in the STX-SPST link is coupled with the LOS ray (if present) in the SPST-SRX link. The resulting path is never dropped. Further, a set  of paths are generated.

* The LOS ray in the STX-SPST link (if present) is coupled with each NLOS ray in the SPST-SRX link.
* Each NLOS ray in the STX-SPST link is coupled with the LOS ray (if present) in the SPST-SRX link.
* The NLOS rays in the STX-SPST link are coupled with the NLOS rays in the SPST-SRX link. Two Options for the coupling are recommended with other methods for complexity reduction up to company choice.
	+ Option 1: Each NLOS ray in the STX-SPST link is coupled with each NLOS ray in the SPST-SRX link.
	+ Option 2: The NLOS rays in the STX-SPST link are 1-by-1 randomly coupled with the NLOS rays in the ST-SRX link. If the number of rays in the two links M1, M2 are not equal, min(M1, M2) rays are randomly selected in the link with larger number of rays in the coupling operation.

Step 10: Obtain the power for all generated paths

The power of a path () is given by

 (7.9-xx)

where, are the second and third component of RCS at the SPST p for a path are derived by the incident angle, i.e., AOA (), ZOA () of the ray in the STX-SPST link and the scattered angle, i.e., AOD (), ZOD () of the ray in the SPST-SRX link, referring to the RCS model defined in Clause 7.9.2.1 for the SPST. are respectively the ray power in the SPST-SRX link and the STX-SPST link.

* If the STX-SPST link is in LOS condition,
	+ for a LOS ray, is the Ricean K-factor of the STX-SPST link.
	+ for a NLOS ray *m* of a stochastic cluster *n,*  , M is number of rays per cluster
* If the STX-SPST link is not in LOS condition,
	+ for a NLOS ray *m* of a stochastic cluster *n*, , M is number of rays per cluster
* If the SPST-SRX link is in LOS condition,
	+ for a LOS ray, , is the Ricean K-factor of the SPST-SRX link.
	+ for a NLOS ray *m’* of a stochastic cluster *n’*,
* If the SPST-SRX link is not in LOS condition,
	+ for a NLOS ray *m’* of a stochastic cluster *n’*,

A path with power less than [-40dB] compared to the maximum power among all paths in set is dropped. The set of remaining paths () after path dropping is denoted as set *R*. The path that couples the LOS ray in the STX-SPST link and the LOS ray in the SPST-SRX link, if present, is included in set R.

Step 11: Obtain the absolute delay for each path in set *R*

The absolute delay of a path () is given by

 (7.9-xx)

where, for the LOS ray in the STX-SPST link, if present, . For the LOS ray in the SPST-SRX link, if present, . is the 3D distance between STX and SPST *p*. is the 3D distance between SPST *p* and SRX. are generated separately for NLOS rays in the SPST-SRX link and the STX-SPST link for bistatic sensing mode, according to Clause 7.6.9. For the two strongest clusters in each of the STX-SPST link and SPST-SRX link, and of sub-clusters are revised according to equation (7.5-26). For monostatic sensing mode, is equal to . are set to 0 for the LOS ray, if present, in the SPST-SRX link and the STX-SPST link.

Step 12: Generate the cross polarization power ratios for paths in set *R*.

The cross polarization power ratios for each ray *m* of a cluster *n* in a STX-SPST link is generated using Step 9 of Clause 7.5, i.e., =.

The cross polarization power ratios for each ray *m’* of a cluster *n’* in a ST-SRX link is generated using Step 9 of Clause 7.5 by replacing subscript *n, m* with *n’, m’*, i.e., .

For monostatic sensing mode, is equal to if and .

Generate the cross polarization power ratios (XPR) for each path in set R at SPST *p*. XPR is log-Normal distributed. Draw XPR values as

 , (7.9-xx)

where is Gaussian distributed with and from Table 7.9.2.2. Note: is independently drawn for each path in set R.

The outcome of Steps 1-12 shall be identical for all the links from co-sited sectors to a STX/ST/SRX.

**Coefficient generation:**

Step 13: Draw initial random phases for paths in set *R*.

The random initial phases for each ray *m* of a cluster *n* in a STX-ST link is generated using Step 9 of Clause 7.5, i.e.,

The random initial phases for each ray *m’* of a cluster *n’* in a ST-SRX link is generated using Step 9 of Clause 7.5 by replacing subscript *n, m* with *n’, m’*, i.e., .

[For monostatic sensing mode, are respectively equal to , if and .]

Draw random initial phases for each path in set *R* at SPST *p* and for four different polarisation combinations (θθ, θϕ, ϕθ, ϕϕ). The distribution for initial phases is uniform within (*-π, π*).

Step 14: Generate channel coefficients for paths in set *R* for each receiver and transmitter element pair *u, s*.

The channel coefficient for a path in set *R* is generated by

(7.9-xx)

with the Doppler frequency defined as

 (7.9-xx)

where,

* is the polarization matrix of the SPST *p*.

 (7.9-xx)

* is the polarization matrix of the ray in the STX-SPST link.
	+ for the LOS ray, if present,
	+ for NLOS ray generated by stochastic cluster,

 (7.9-xx)

* is the polarization matrix of th ray in the SPST-SRX link.
	+ for the LOS ray, if present,
	+ for NLOS ray generated by stochastic cluster,

 (7.9-xx)

* are the two elements in the main diagonal of matrix
* is the spherical unit vector at receiver for the link from SRX to SPST *p* of ST *k*, given by

 (7.9-xx)

* is the spherical unit vector at transmitter for the link from STX to SPST *p* of ST *k*, given by

 (7.9-xx)

* is the spherical unit vector at the scattering point for the link from SPST *p* of ST *k* to SRX, given by

 (7.9-xx)

* is the spherical unit vector at the scattering point for the link from SPST *p* of ST *k* to STX, given by

 (7.9-xx)

* are respectively the velocity of SRX, STX
* is the velocity of SPST *p* of ST *k*, , where is the velocity of the ST *k*, is velocity due to micro motion of SPST *p* of ST *k*
* denotes a reference point in time that defines the initial phase, e.g. .

The channel impulse response of SPST *p* of ST *k* is given by

 (7.9-xx)

Step 15: Apply pathloss, shadowing, the first component of RCS for the channel coefficients.

The target channel for ST *k*, is formed by summing the channel coefficients of the *P* SPST respectively scaled by the pathloss, shadowing and the first component of RCS of the *P* SPST*.*

 (7.9-xx)

Where,

* is the pathloss of the STX-SPST link
* is the pathloss of the SPST-SRX link
* is the shadow fading of the STX-SPST link
* is the shadow fading of the SPST-SRX link
* is the first component of RCS for the SPST *p* of ST *k*, referring to the RCS model defined in Clause 7.9.2.1,
* , *P* is the total number of SPST of the ST *k*.

#### 7.9.4.2 Background channel

For TRP-TRP, TRP-UE, UE-TRP and UE-UE bistatic sensing modes, following Step 1 in Clause 7.9.4.0, the background channel between a pair of STX and SRX is generated using Step 2-12 of Clause 7.5 with parameters derived by Table 7.9.3-3. The absolute time of arrival in clause 7.6.9 is applied. The resulting channel is denoted as .

For TRP monostatic and UE monostatic sensing modes, the background channel between a pair of STX and SRX is generated using the following steps after Step 1 in Clause 7.9.4.0.

Step 2: Generate 3 reference points (RPs) for the STX/SRX

Draw the distance between the STX/SRX and each RP, the height of each RP respectively from Gamma distribution and defined in Table 7.9.4.2-1/2. With uniform distribution within range , draw the LOS AOD (*ϕLOS,AOD*) between the STX/SRX and the first RP. The LOS AOD is further rotated by and to respectively derive the LOS AOD from the STX/SRX to the second and third RPs. Consequently, the 3D location of each RP can be calculated.

* Determine LOS ZOD (*θLOS,ZOD*), LOS AOA (*ϕLOS,AOA*), and LOS ZOA (*θLOS,ZOA*) of the STX/SRX and each RP in the global coordinate system.
* Set each RP the same antenna field patterns *Frx* in the global coordinate system and array geometries as the STX/SRX
* Set each RP the same array orientations with respect to the global coordinate system, i.e., Ω*RP,α* (RP bearing angle), Ω*RP,β* (RP downtilt angle) and Ω*RP,γ* (RP slant angle) as the STX/SRX.

Step 3: Assign NLOS propagation condition to the channel between the STX/SRX and each of the 3 RPs.

Step 4: Generate the channel between the STX/SRX and each of the 3 RPs using Step 3-12 of Clause 7.5 with parameters derived by Table 7.9.3-3, unless stated otherwise.

* In Step 7 of Clause 7.5, the arrival angles are respectively equal to departure angles . The rays in a cluster with less than [50, 60 and 90] degrees respectively for scenario UMi, UMa and RMa are dropped. The dropping is not applicable to other sensing scenarios.
* The absolute time of arrival [in clause 7.6.9] is applied [with the following updates]. The same is generated and applied to the 3 channels between the STX/SRX and the 3 RPs.

Step 5: Generate the background channel for the STX/SRX

The background channel for the STX/SRX is formed by summing the 3 channels between STX/SRX and the 3 RPs after applying the respective pathloss and shadowing.

Where,

* is the pathloss between the STX/SRX and the RP with index r
* is the shadow fading between the STX/SRX and the RP with index r

Table 7.9.4.2-1: Parameters of background channel for TRP monostatic sensing

| Scenarios | UMi | UMa | RMa | InH | InF |
| --- | --- | --- | --- | --- | --- |
| Distance | αd |  |  |  |  |  |
| βd |  |  |  |  |  |
| cd |  |  |  |  |  |
| Height | αh |  |  |  |  |  |
| βh |  |  |  |  |  |
| ch |  |  |  |  |  |

Table 7.9.4.2-2: Parameters of background channel for UT monostatic sensing

| Scenarios | UMi | UMa | RMa | InH | InF |
| --- | --- | --- | --- | --- | --- |
| Distance | αd |  |  |  |  |  |
| βd |  |  |  |  |  |
| cd |  |  |  |  |  |
| Height | αh |  |  |  |  |  |
| βh |  |  |  |  |  |
| ch |  |  |  |  |  |

#### 7.9.4.3 Combining target channel and background channel

The channel model for ISAC for a pair of STX and STX is the sum of the target channel(s) and the background channel generated in Clause 7.9.4.1 and 7.9.4.2, i.e.,

. (7.9-xx)

### 7.9.5 Additional modelling components

#### 7.9.5.1 Spatial consistency

The spatial consistency procedure is used to generate the random variables for the STX-SPST links, the SPST-SRX links and the background channels, so that they are spatial consistent. The spatial consistency procedures in Clause 7.6.3 are reused to handle the links between TRPs and STs/UTs.

For sensing scenario UMi-AV, UMa-AV and RMa-AV, the 2D random process (in the horizontal plane) can be extended to 3D random process [with vertical correlation distance]. The random coupling of NLOS rays of Option 2 in Step 9 in Clause 7.9.4.1 shall be kept unchanged per simulation drop even if STX/ST/SRX position(s) changes during simulation.

A new spatial consistency procedure is provided for the large scale parameter, cluster specific parameters and ray specific parameters of the links between UT and UT/SPSTs (denoted as UT-UT/SPST links).

* Link-correlated: parameters of any two links of UT-UT/SPST links are correlated, subjected to correlation distance.
* All-correlated: all UT-UT/SPST links are correlated.

In Table 7.9.5.1-1, correlation type for each parameter of the new spatial consistency procedure is clarified.

Table 7.9.5.1-1: Correlation type among UT-UT/SPST links

|  |  |
| --- | --- |
| Parameters | Correlation type |
| Delays | Link-correlated |
| Cluster powers | Link-correlated |
| AOA/ZOA/AOD/ZOD offset | Link-correlated |
| AOA/ZOA/AOD/ZOD sign | Link-correlated |
| Random coupling | Link-correlated |
| XPR | Link-correlated |
| Initial random phase | Link-correlated |
| LOS/NLOS states | Link-correlated |
| Blockage (Model A) | All-correlated |
| O2I penetration loss | All-correlated |
| Indoor distance | All-correlated |
| Indoor states | All-correlated |

Spatial consistency is not modelled among STX-SPST links, the SPST-SRX links and the background channels in the following situations:

- Different link types, e.g., outdoor LOS, outdoor NLOS or O2I, as defined in Table 7.6.3.4-2

- UE locates on different floors, as defined in Table 7.6.3.4-2

- Background channel for monostatic sensing mode, and any link (STX-SPST link, SPST-SRX link, background channel) for bistatic sensing mode

- Links associated with different non-co-located TRPs, e.g. TRP1-ST/UT/TRP and TRP2-ST/UT/TRP.

#### 7.9.5.2 Type-2 environment object

A type-2 EO, e.g., wall, is modelled as a surface with finite size. A ray specularly reflected by a type-2 EO can be modelled in the STX-SPST link, SPST-SRX link [and/or the background channel], if a specular reflection point can be found within the surface of the type-2 EO.

A general procedure to generated small scale parameters of a type-2 EO, e.g., a wall, is provided assuming the incident ray comes from Tx and the scattered ray arrives at Rx.

Step A: Check whether a ray specularly reflected by a type-2 EO needs to be modelled or not for the pair of Tx and Rx

The type-2 EO can be described by a plane equation perpendicular to the ground.

 (7.9-xx)

[A, B] is the normal vector of the plane, which points to the same direction as the orientation of the type-2 EO. The location of Tx and Rx is denoted as and .

If or , there is no reflection path in the Tx-Rx link due to the type-2 EO. Otherwise, the location of reflection point is determined as follows.

 (7.9-xx) (7.9-xx) (7.9-xx)

Where, is the location of the reflection image of Tx relative to the plane. . .

If , the reflection point is on the surface of the type-2 EO, otherwise, there is no reflection path in the Tx-Rx link due to the type-2 EO.

Step B: Generate parameters of the ray specularly reflected by a type-2 EO if the reflection point is only the surface of the type-2 EO

The 3D distance from the Tx to the reflection point then to the Rx is

 (7.9-xx)

The ZoD and AoD from Tx to the reflection point are derived based on the location of Tx and reflection point.

 (7.9-xx)

 (7.9-xx)

The ZoA and AoA from Rx to the reflection point are derived based on the location of Rx and reflection point.

 (7.9-xx)

 (7.9-xx)

The effective polarization matrix of the type-2 EO reflection path is given by

 (7.9-xx)

Where,

* . represents the normal vector of the incident plane. , in which and . represents the spherical basis vector of incident ray in vertical direction. represents the spherical basis vector of incident ray in horizontal direction..
* . represents the polar basis vector of scattering ray in vertical direction. represents the polar basis vector of scattering ray in horizontal direction. . .
* The formula 7.6-38 and 7.6-39 of reflection coefficients and in Clause 7.6.8 can be reused with modified incidence angle. The incidence angle is the angle between the incident vector from Tx to the reflected point and the normal vector, which is

The reflection coefficients for parallel and perpendicular polarization are given by

When a type-2 EO is deployed in the simulation area, the following modification to the ISAC channel generation in Clause 7.9.4, 7.9.4.1 and 7.9.4.2 can be applied.

1. In Step 1 in Clause 7.9.4.0,

b) Give number of type-2 EO, additionally.

c) Give 3D locations of type-2 EO in the global coordinate system, additionally.

e) Give the orientation of type-2 EO in the global coordinate system, additionally. The type-2 EO orientation is defined by three angles Ω*EO,α* (type-2 EO bearing angle), Ω*EO,β* (type-2 EO downtilt angle) and Ω*EO,γ* (type-2 EO slant angle).

Note: In case wrapping is used, each wrapping copy of a type-2 EO should be treated as a separate type-2EO considering channel generation.

1. [In Step 2 in Clause 7.9.4.1, ]

[Rapporteur’s note: Further agreement necessary regarding LOS condition when Type-2 EO is present.]

1. Between Step 8 and 9 in Clause 7.9.4.1, insert one step to generate NLOS rays specularly reflected by type-2 EO, if present.

In a STX-SPST link, the general procedure to model a type-2 EO as described above is executed by substitute Tx with the STX and Rx with the SPST. A NLOS ray specularly reflected by a EO type-2, if present, is represented by . .

In a SPST-SRX link, the general procedure to model a type-2 EO as described above is executed by substitute Tx with the SPST and Rx with the SRX. A NLOS ray specularly reflected by a EO type-2, if present, is represented by . .

1. In Step 9 in Clause 7.9.4.1,

The following paths are generated and added to set .

* A NLOS ray specularly reflected by type-2 EO, if present in the SPST-SRX link is coupled with a NLOS ray specularly reflected by type-2 EO, if present in the STX-SPST link
* A NLOS ray specularly reflected by type-2 EO, if present in the SPST-SRX link is coupled with any LOS ray (if present) and NLOS rays of stochastic clusters in the STX-SPST link
* A NLOS ray specularly reflected by type-2 EO, if present in the STX-SPST link is coupled with any LOS ray (if present) and NLOS rays of stochastic clusters in the SPST-SRX link
1. In Step 10 in Clause 7.9.4.1,

 for a NLOS ray specularly reflected by a type-2 EO, if present, in the SPST-SRX link and the STX-SPST link is determined as follows.

* If the STX-SPST link is in LOS condition,
* If the STX-SPST link is not in LOS condition, [TBD]
* If the SPST-SRX link is in LOS condition,
* If the SPST-SRX link is not in LOS condition, [TBD]
1. In Step 11 in Clause 7.9.4.1,

For a NLOS ray specularly reflected by a type-2 EO in the STX-SPST link, if present, is replaced by , and is set to 0.

For a NLOS ray specularly reflected by a type-2 EO in the SPST-SRX link, if present, is replaced by , and is set to 0.

1. The outcome of Steps 1-12 in Clause 7.9.4.1 shall be identical for all the links from co-sited sectors to a STX/ST/EO/SRX.

[Rapporteur’s note: Further agreement necessary regarding Type-2 EO in background channel.]

1. [In Clause 7.9.4.2, if type-2 EO is present, a ray specularly reflected by a type-2 EO is generated if a specular reflection point can be found within a surface of the EO.]

#### 7.9.5.3 Power normalization across target channel and background channel

[Rapporteur’s note: further agreements are necessary on model B with power normalization]

To combine the target channel and the background channel, an alternative scheme of power normalization can be applied to keep the same/similar channel power as the background channel without sensing target.

#### 7.9.5.4 Doppler of mobile scatters

To support scatterer mobility, the Doppler frequency component in the channel coefficient generation in step 13 in clause 7.9.4.1 should be updated as follows.

 (7.9-xx)

Where,

* is a random variable from to , and is the maximum speed of the clutter. is a random variable of Bernoulli distribution with mean if , otherwise . Parameter determines the proportion of mobile scatterers and can thus be selected to appropriately model statistically larger number of mobile scatterers (higher ) or statistically smaller number of mobile scatterers (e.g. in case of a completely static environment: =0 results in all scatteres having zero speed). [A typical value of is 0.2].
* is a random variable from to , and is the maximum speed of the clutter. is a random variable of Bernoulli distribution with mean *p* if , otherwise . Parameter *p* determines the proportion of mobile scatterers and can thus be selected to appropriately model statistically larger number of mobile scatterers (higher *p*) or statistically smaller number of mobile scatterers (e.g. in case of a completely static environment: p=0 results in all scatteres having zero speed). [A typical value of *p* is 0.2].

#### 7.9.5.5 Lower power clusters

In addition to the clusters/rays in background channel generated in Clause 7.9.4.2, more clusters/rays can be generated to simulate the weak rays in the background channel which still impacts the sensing performance. The following procedure is applicable for bistatic sensing or for monostatic sensing.

Step 1: Generate a first background channel according to Clause 7.9.4.2.

Step 2: Generate a second background channel according to Clause 7.9.4.2 with the following revised parameters: 1) The number of clusters (N in Clause 7.5) is increased to 360; 2) The number of ray per cluster (M in Clause 7.5) is reduced to 1.

Step 3: The power of the clusters/rays in the second background channel is scaled down by , and is added to the first background channel, where, dB,  is the maximum power of the NLOS clusters in the first background channel. The final background channel is

 (7.9-xx)

### 7.9.6 Channel models for link-level evaluations

[Rapporteur’s note: this clause is to capture the agreements on LLS channel model for ISAC.]

### 7.9.7 Channel model calibration

#### 7.9.7.1 Large scale calibration

For the purposes of large scale calibration without fast fading modelling for sensing targets UAV, [human], automotive and [AGV], the calibration parameters are respectively provided in Table 7.9.7.1-1/2/3/4. Unspecified parameters in Table 7.9.7.1-2/3/4 are the same as those in Table 7.9.7.1-1. The calibration results based on xxxx can be found in R1-xxxxxx.

**Table 7.9.7.1-1: Simulation assumptions for large scale calibration for UAV sensing targets**

|  |  |
| --- | --- |
| **Parameters** | **Values** |
| Scenario | UMa-AV |
| Sensing mode | TRP monostatic, TRP-TRP bistatic, TRP-UE bistatic, UE-UE bistatic |
| Target type | UAV of small size (0.3m x 0.4m x 0.2m) |
| Sectorization | Single 360-degree sector can be assumed |
| Carrier Frequency | FR1: 6 GHzFR2: 30 GHz |
| BS antenna configurations | Single dual-pol isotropic antenna |
| BS Tx power | FR1: 56dBmFR2: 41dBm |
| Bandwidth | FR1: 100MHzFR2: 400MHz |
| BS noise figure | FR1: 5dBFR2: 7dB |
| UT antenna configurations | Single dual-pol isotropic antenna; (M,N,P,Mg,Ng;Mp,Np) = (1,1,2,1,1;1,1) |
| UT noise figure | FR1: 9dBFR2: 10dB |
| UT height | 1.5m for terrestrial UTs,  |
| UT Tx power | 23dBm |
| UT Distribution | • The overall number of UTs is 30 uniformly distributed in the center cell. • All of the UTs are either terrestrial UTs or aerial UTs, all outdoors. • Vertical distribution of aerial UE: Fixed height value of 200 m.• FR1 is assumed for aerial UE. |
| Sensing target distribution | 1target uniformly distributed (across multiple drops) within the center cell. Vertical distribution: Fixed height value of 200 m. |
| Component A of the RCS for each scattering point | -12.81 dBsm  |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | 10 m |
| Wrapping Method | No wrapping method is used if interference is not modelled, otherwise geographical distance based wrapping |
| Coupling loss for target channel | power scaling factor (pathloss, shadow fading, and RCS component A included): |
| Sensing Tx/Rx selection | Best N = 4 Tx-Rx pairs to be selected for the target. NOTE1: Based on the Tx-Rx pairs with the smallest power scaling factor of the target channel.  |
| Metrics | Coupling loss for target channel Coupling loss for background channel (in case of monostatic sensing, this is the coupling loss between Tx and one reference point)Note: CDFs can be separately generated for target channel, background channel  |

**Table 7.9.7.1-2. Simulation assumptions for large scale calibration for Human sensing targets**

**Table 7.9.7.1-3. Simulation assumptions for large scale calibration for Automotive sensing targets**

|  |  |
| --- | --- |
| **Parameters** | **Values** |
| Scenario | For FR1:Urban Grid (ISD=500m, BS height=25m) Highway (ISD=1732m, BS height=35m)For FR2:Urban Grid (ISD=250m, BS height=25m) Highway (ISD=500m, BS height=35m) |
| Sensing mode | TRP monostatic, TRP-TRP bistatic, TRP-UE bistatic, UE-UE bistatic, UE monostatic |
| Target type | Vehicle type 2 [TR37.885] |
| UT Distribution | Per TR37.885 |
| Sensing target distribution | Per TR37.885:- Option A- Vehicle type distribution: 100% vehicle type 2.- Clustered dropping is not used.- Highway: one target uniformly distributed (across multiple drops) within the simulation region. Vehicle speed is 140 km/h in all the lanes as baseline.- Urban Grid: one target is uniformly distributed (across multiple drops) within the center road grid. Vehicle speed is 60 km/h in all the lanes as baseline.NOTE: vehicle is dropped with 5 scattering points (front/left/right/back/roof) and each point has one location, or vehicle is dropped with 1 scattering points |
| Component A of the RCS for each scattering point | -20dBsm |
| Minimum 3D distances between pairs of Tx/Rx and sensing target | 10 m  |
| Wrapping Method | As defined in urban grid/highway scenario |

**Table 7.9.7.1-4. Simulation assumptions for large scale calibration for AGV sensing targets**

#### 7.9.7.2 Full calibration

For the purpose of full calibration including the fast fading modelling for sensing scenarios UAV, [human], automotive and [AGV], the calibration parameters are respectively provided in Table 7.9.7.2-1/2/3/4. Unspecified parameters in the tables are the same as those in Table 7.9.7.1-1. The calibration results based on xxxx can be found in R1-xxxxx.

**Table 7.9.7.2-1. Simulation assumptions for full calibration for UAV sensing targets**

|  |  |
| --- | --- |
| **Parameters** | **Values** |
| Scenario | UMa-AV |
| Sensing mode | TRP monostatic, TRP-TRP bistatic, TRP-UE bistatic, UE-UE bistatic |
| Target type | UAV of small size (0.3m x 0.4m x 0.2m) |
| RCS for each scattering point | Component A: -12.81 dBsmComponent B1: 0 dBComponent B2: 3.74 dB for standard deviationThe same values are used for monostatic RCS and bistatic RCS |
| Fast fading model  | TR 36.777 Annex B.1.3  |
| (u, std) for XPR of target | Mean 13.75 dB, deviation 7.07 dB |
| The power threshold for path dropping after concatenation for target channel | FFS |
| Coupling loss for target channel | By definition, need to consider all direct and indirect paths. The following parameters are included in the calculation:* power scaling factor (pathloss, shadow fading, and RCS component A included)
* for small scale

RCS B1/B2 and power of rays in Tx-target/target-Rx links (), Tx/Rx antenna pattern, 3 polarization matrixes, i.e.,  |
|  |
| Absolute delay | The model of UMa scenario defined in TR 38.901 7-24GHz channel modeling [ref] is reused for UMa-AV for all sensing modes. |
| Metrics | Coupling loss for target channel Coupling loss for background channel (in case of monostatic sensing, this is the linear sum of coupling losses between Tx/Rx and all reference points)Note: CDFs can be separately generated for target channel, background channelCDF of Delay Spread and Angle Spread (ASD, ZSD, ASA, ZSA). Definition of Delay Spread is similar to the definition of angle spread in Annex A of TR 25.996, Definition of Angle Spread can ref to Annex A of TR 25.996. |

**Table 7.9.7.2-2. Simulation assumptions for full calibration for Human sensing targets**

**Table 7.9.7.2-3. Simulation assumptions for full calibration for Automotive sensing targets**

**Table 7.9.7.2-4. Simulation assumptions for full calibration for AGV sensing targets**

#### [7.9.7.3 Calibration of additional features]

[Rapporteur’s note: if agreed, this clause is to capture the agreements on calibration assumptions/results for additional features.]

**< Unchanged text omitted >**

**< Unchanged text omitted >**